

Test Report: DX Engineering DXE-RPA-1 Wideband Preamplifier

By Adam Farson VA7OJ/AB4OJ, 3 October 2013

1. **Noise Power Ratio (NPR).** The DUT was powered from +13.8V DC and connected between the RS-50 White Noise Generator and the RE-50 Noise Receiver via 75Ω coax. These instruments form the Wandel & Goltermann RK-50 Noise Test Set. In the RS-50, the 60-4100 kHz BPF and 3886 kHz bandstop filter were selected; in the RE-50, the 3886 kHz down-converter was selected. NPR was measured over the noise loading range -50 to -5 dBm. Results per **Table 1**.

Table 1: Noise Power Ratio (NPR).

| BPF kHz | Bandstop kHz | P _{TOT} (Noise Loading) dBm | NPR dB | NPR (dB) at V _{CC} = +15V |
|---------|--------------|--------------------------------------|--------|------------------------------------|
| 60-4100 | 3886 | -50 | 52 | |
| | | -40 | 62 | |
| | | -30 | 71 | |
| | | -20 | 77 | |
| | | -10 | 76 | |
| | | -5 | 65 | 68 |
| | | 0 | 29 | 31.5 |

2. **Gain:** The DUT was connected between a signal source and an RF power meter as follows: Marconi 2019 signal generator ► MCL FT1.5-1B 50/75Ω transformer ► DUT ► MCL FT1.5-1C 75/50Ω transformer ► Millivac MV-723B RF millivoltmeter w/50Ω terminated probe. V_{CC} was +13.8V. Input power was increased until ≈ 3 dB compression was observed. (See **Table 2**.)

Table 2: Gain.

| f MHz | P _{IN} dBm | P _O dBm | Gain dB |
|-------|---------------------|--------------------|---------|
| 1.8 | -30.7 | -14.5 | 16.2 |
| | -20.7 | -4.5 | 16.2 |
| | -10.7 | +14 | 16.7 |
| | -0.7 | +15 | 15.7 |
| | +9.3 | +24.5 | 15.2 |
| | +12.3 | 25 | 12.7 |

Note: At V_{CC} = +13.8V, P_O & gain decreased by 0.5 dB.

3. **Third Order Intercept (IP₃):** The Marconi 2018A (f₁) and 2019 (f₂) signal generators were connected, each via a 10 dB pad, to an MCL ZSC-2-2 combiner followed by a 0 – 110 dB step attenuator and a MCL FT1.5-1B 50/75Ω transformer. The 75Ω output was connected to the DUT, which drove an HP 8563E spectrum analyser via an MCL FT1.5-1C 75/50Ω transformer and a 15 dB pad. The HP 8563E had the HP 85672A Spurious Response Utility installed.

Input power was -1 dBm/tone, and output was +15 dBm/tone. 2-tone IP₃ was measured at 1.8 MHz, and at 2, 50 and 150 kHz test-signal spacing. The test results are given in the following charts.

DXE-RPA-1 Preamp (VE7KW). Actual output +15 dBm/tone. 2 kHz spacing. 03.10.2013.

| INTERMODULATION | | MEASUREMENT | | RESULTS | |
|-----------------|----------|-------------|-----|---------|-----|
| LOWER | SIGNAL: | 1.810 | MHz | -3 | dBm |
| UPPER | SIGNAL: | 1.812 | MHz | -5 | dBm |
| SIGNAL | SPACING: | 2.000 | kHz | | |
| IMD | (LOWER | PRODUCT): | | -66.5 | dBc |
| IMD | (UPPER | PRODUCT): | | -66.3 | dBc |
| TOI/IP3 | (LOWER | PRODUCT): | | 32.8 | dBm |
| TOI/IP3 | (UPPER | PRODUCT): | | 32.8 | dBm |

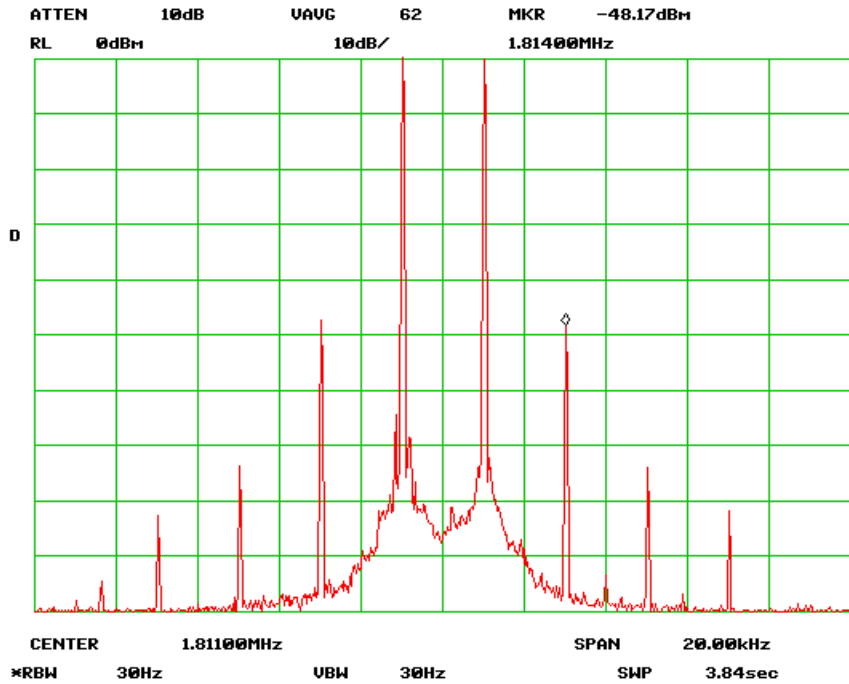
DXE-RPA-1 Preamp (VE7KW). Actual output +15 dBm/tone. 50 kHz spacing. 03.10.2013.

| INTERMODULATION | | MEASUREMENT | | RESULTS | |
|-----------------|----------|-------------|-----|---------|-----|
| LOWER | SIGNAL: | 1.810 | MHz | 0 | dBm |
| UPPER | SIGNAL: | 1.860 | MHz | -2 | dBm |
| SIGNAL | SPACING: | 50.00 | kHz | | |
| IMD | (LOWER | PRODUCT): | | -66.3 | dBc |
| IMD | (UPPER | PRODUCT): | | -68.2 | dBc |
| TOI/IP3 | (LOWER | PRODUCT): | | 33.1 | dBm |
| TOI/IP3 | (UPPER | PRODUCT): | | 34.0 | dBm |

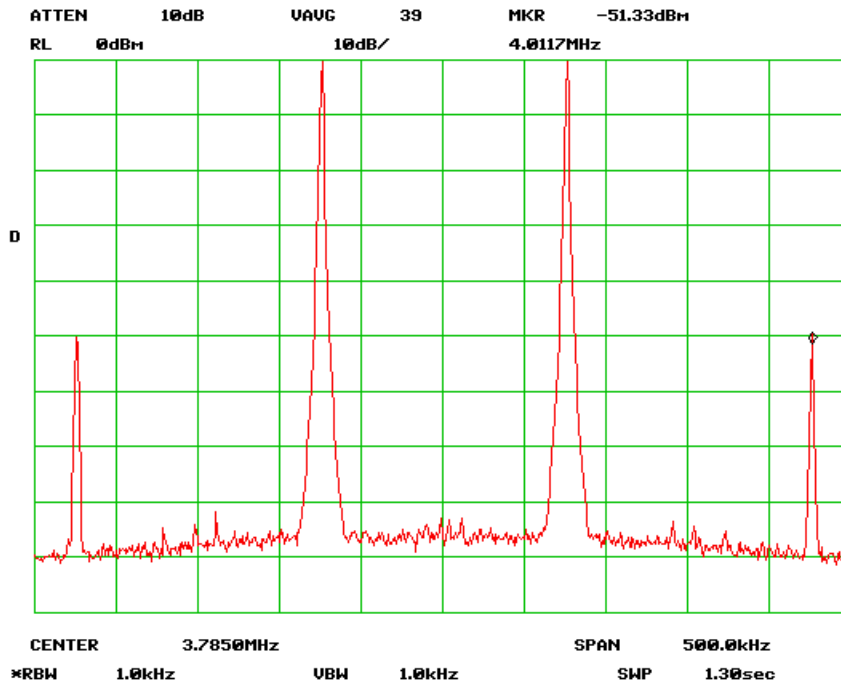
DXE-RPA-1 Preamp (VE7KW). Actual output +15 dBm/tone. 150 kHz spacing. 03.10.2013.

| INTERMODULATION | | MEASUREMENT | | RESULTS | |
|-----------------|----------|-------------|-------|---------|-----|
| LOWER | SIGNAL: | 3.710 | MHz | 0 | dBm |
| UPPER | SIGNAL: | 3.860 | MHz | -0.2 | dBm |
| SIGNAL | SPACING: | 150.0 | kHz | | |
| IMD | (LOWER | PRODUCT): | -66.3 | dBc | |
| IMD | (UPPER | PRODUCT): | -66.0 | dBc | |
| TOI/IP3 | (LOWER | PRODUCT): | 33.1 | dBm | |
| TOI/IP3 | (UPPER | PRODUCT): | 32.9 | dBm | |

DXE-RPA-1 Preamp (VE7KW). Actual output +15 dBm/tone. 2 kHz spacing. 03.10.2013.



DXE-RPA-1 Preamp (VE7KW). Actual output +15 dBm/ tone. 150 kHz spacing. 03.10.2013.



4. **Noise Figure(NF):** NF was measured by the “modified Y-Factor” method, using the following test setup: NoiseCom NC6110 noise generator ► 0-110 dB step attenuator ► MCL BLP-30 30 MHz LPF MCL FT1.5-1B 50/75Ω transformer ► DUT ► MCL FT1.5-1C 75/50Ω transformer ► MCL GALI-74* wideband amplifier ► 2 dB pad ► HP 8563E spectrum analyser. V_{CC} was +13.8V.

Spectrum analyser settings: Centre freq. 14.100 MHz; span 1 kHz; reference level -10 dBm; RBW = 3 Hz; VBW = 1 Hz; DET = Sample; MKRNOISE On; Video averaged; read at 50 averagings.

*GALI-74 has 2.9 dB NF, 21 dB gain.

1. Read marker level with noise OFF and DUT input terminated (-131.5 dBm). This corresponds to the noise output of a 75Ω resistor at room temperature (“cold”).
2. Turn noise ON, and adjust attenuator for ≈ 10 dB increase in marker amplitude. Read marker amplitude again (“hot”) and record attenuator setting. Subtract “cold” from “hot” marker amplitude to obtain ΔN .
3. Calculate NF:

$$NF = \text{Noise density of generator} - \text{attenuator setting} + 174 - \Delta N$$

For our test, noise density of generator = -82 dBm/Hz; attenuator setting was 77 dBm; $\Delta N = 9.8$ dB.

Thus $NF = -82 - 77 - 1^{**} + 174 - 9.8 = 4.2$ dB. (DXE spec is 3.5 dB). There will be a slight error due to the residual NF of the spectrum analyser behind the GALI-74 amplifier. **** Insertion loss of matching transformers.**

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